

# Biodiesel production from rice bran oil over modified natural zeolite catalyst

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## BIODIESEL PRODUCTION FROM RICE BRAN OIL OVER MODIFIED NATURAL ZEOLITE CATALYST

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### ABSTRACT

The purpose of this study is to develop natural zeolite impregnated with potassium nitrate (KNO<sub>3</sub>) a heterogenous catalyst for the transesterification of rice bran oil (RBO) in order to produce Fatty Acid Methyl Ester (FAME). We conducted the Nitrogen adsorption-desorption method, Fourier Transform Infra-Red (FT-IR) spectrometer, and X-Ray Diffraction (XRD) analysis in order to characterize the physicochemical properties of the modified natural zeolite catalysts. We investigated the influences of RBO to methanol mole ratio in the range of 1:6 to 1:12. The variation of natural zeolite catalyst amount performed, also, at 1, 2.5, 5 and 10 wt. % of RBO. Moreover, the reaction temperatures were varied at room temperature (32°C), 60°C and 67.5°C. The highest biodiesel yield was 83.2% which was obtained at a ratio of 1:12 RBO to methanol mole, an amount of modified natural zeolite catalyst of 10 wt.% of RBO and a reaction temperature of 67.5°C. In order to study the reusability of modified natural zeolite catalyst, three successive transesterification reactions were carried out using the same reaction conditions.

**Keywords:** Biodiesel; Catalyst; Natural zeolite; Potassium; Rice bran oil (RBO)

### 1. INTRODUCTION

Biodiesel is an alternative fuel that contains long chain fatty acids mono alkyl ester. The raw materials, used in producing biodiesel, originate from natural sources i.e. vegetable oils or animal fat (Pradana et al., 2017). Biodiesel can replace fossil fuels in conventional diesel engines. Biodiesel is predominantly a renewable, clean burning fuel that is environmentally friendly, non-toxic, and free from harmful sulphur (Chen et al., 2011). Biodiesel synthesis can be carried out by either the esterification of fatty acids or the transesterification process of triglycerides contained in the raw materials.

The cost of production process is a major constraint related to the commercialization of biodiesel production. The use of low cost feedstock is an alternative way of improving the economic value of biodiesel production and its commercial production industry scale. Rice bran oil (RBO) is the vegetable oil that has the potential as a low cost feedstock for biodiesel production. RBO was obtained from rice milling. The extraction of the hard outer brown layer of rice after rice husk is the process used to generate RBO. Approximately the RBO content in rice bran is 15–23% of weight which is determined from the type of rice and milling process. As an agricultural country, Indonesia has the potential to generate annually RBO on a large scale. In 2016, Indonesia produced about 75 million tons of rice bran with a potential of yielding 15 million tons of RBO. Due to the high oil content, it is proposed that RBO has the prospect of becoming a predominant

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low-cost feedstock for Indonesian biodiesel production. Conventionally, by using either transesterification or the esterification process, the homogeneous base or acid catalysts are employed in biodiesel production. However, there are many obstacles to using homogeneous catalysts for biodiesel production; these are such as the need for a further product separation process, the catalysts are used only once, and they produce hazardous waste. Therefore, in order to overcome the problems, there has been widespread reporting of heterogeneous catalysts being an alternative procedure in biodiesel production (Yusuff et al., 2018). The heterogeneous catalysts have many advantages i.e. easy separation from the biodiesel product (Takagaki, et al., 2006), reusability (Mardhiah et al., 2017) and generation of harmless waste (Alonso et al., 2007).

There have been reports about a number of solid catalysts in relation to their transesterification reactions. These are such as calcium lanthanum/CaO–La<sub>2</sub>O<sub>3</sub> mixed oxide catalyst (Taufiq-Yap et al., 2014), anion exchange resin (Jaya et al., 2015), Li–Al mixed oxide catalyst/LiAlO<sub>2</sub> (Dai et al., 2015), ZrMgAl hydrotalcites (Nowicki et al., 2016), Na/Zr-SBA-15 (Chen et al., 2014), KOH/ZSM<sub>5</sub> (Saba et al., 2016), Ce/Mn oxide catalyst (Nasreen et al., 2016), strontium-doped CaO/MgO catalyst (Sudsakorn et al., 2017), tetraalkylammonium hydroxide-functionalized SBA-15 materials (Xie & Fan, 2014), Amine-functionalized MCM-41 catalysts (de Lima et al., 2014), sugarcane bagasse (Augustia et al., 2018), coconut shell biochar (Hidayat et al., 2015, Hidayat et al., 2016), rice husk ash (Hidayat & Sutrisno, 2017) and tin catalysts (Shah et al., 2014).

Natural zeolite, which is an abundant and low-cost resource, is a type of frame-structured hydrated aluminosilicate mineral. The structures of natural zeolites consist of three-dimensional frameworks of SiO<sub>4</sub> and AlO<sub>4</sub> tetrahedral. Commonly, in many industries, zeolites have been applied as either ion-exchange resin or wastewater treatment or molecular sieve or solid catalyst. As catalysts, Zeolites have the characteristics of acidic sites and shape selectivity. Due to the its porous structure, the ability for small molecules such as triglycerides to enter the inner structure, chemical and thermal stability and relatively low cost, the natural zeolite can be utilized as a solid catalyst for biodiesel synthesis.

There have been studies of utilizing zeolite as a catalyst for biodiesel production through using different types of feedstock such as sunflower oil, soybean oil and palm oil. Al-Jammal et al. (2016) tested zeolite tuft for transesterification reaction of sunflower oil. After 2 hours, the highest yield of biodiesel was 96.7% which was obtained under the following reaction conditions: 1:11.5 oil to methanol mole ratio and 50°C reaction temperatures. In another report, Wu et al. (2013) prepared various types of CaO catalysts, supported by NaZSM-5, KL and NaY zeolites, for the purpose of catalyzing the transesterification reaction of soybean oil. The result showed that the biodiesel yield was 95% under the optimal conditions, namely, 1:9 oil to methanol mole ratio, 3 wt.% catalyst amounts, 65°C reaction temperature and 3 hours reaction time. By using palm oil as feedstocks, Kusuma et al. (2013) tested KOH/natural zeolite for transesterification reaction. The required amount of catalyst was 3 wt.% to reach the maximum biodiesel yield of 97.02% after 3 hours with a reaction temperature of 60°C and palm oil to methanol of 1:7.

Besides technical aspects, the economic analysis plays the important role in determining the feasibility of the biodiesel plant. Also, different authors conducted economic analyses of several biodiesel productions. The numerous selection criteria, which were proposed to determine the economic viability of biodiesel commercialization, were total capital cost (Zhang et al., 2003), net present value (Marchetti & Errazu, 2008), biodiesel break-even price (You et al., 2008) and the rate of return after tax (West et al., 2008). Economic analysis provides a better understanding of the commercialization of biodiesel production and provides, also, a very useful tool to predict limits of economic feasibility.

This research study, we used the transesterification reactions of RBO from potassium nitrate ( $\text{KNO}_3$ ) to support natural zeolite. This study offers the simple preparation procedure to synthesis heterogeneous catalysts by using natural zeolite as a catalyst support because of its abundant availability and low price. The catalysts' activities were tested by varying the RBO to methanol mole ratio, reaction temperatures and the amount of natural zeolite catalyst. The use of RBO gives, also, an alternative resource raw material for biodiesel production.

## 2. METHODOLOGY

### 2.1. Catalyst Preparation

We sieved the natural zeolite support into particles with diameters between 150 and 200 mesh and refluxed them with 0.5 M  $\text{H}_2\text{SO}_4$  solution at  $90^\circ\text{C}$  for 4 hours. The  $\text{H}_2\text{SO}_4$  solution can modify the porous structures and can increase the internal surface area so that it provides more sites on the surface of the natural zeolite surface for occupation by the active metals. Then, we washed the natural zeolite with distilled water to neutralize the materials. Thereafter, we dried the activated natural zeolite in the oven overnight at  $110^\circ\text{C}$ . We purchased the metal salts, Potassium nitrate ( $\text{KNO}_3$ ), from E. Merck (Germany). In order to prepare the catalyst, we applied the incipient wetness impregnation technique to the potassium metals on the natural zeolite surface. We conducted the impregnation methods as follows: a certain amount of natural zeolite was mixed with a  $\text{KNO}_3$  metal salt solution. Then, the mixture was stirred vigorously for 24 hours at ambient temperature. Thereafter, the mixture was filtered and the prepared catalyst was calcined in a muffle furnace at  $400^\circ\text{C}$  for 4 hours. The natural zeolites, which were activated and continued with potassium impregnation, were labelled as the K/NZ catalysts.

### 2.2. Catalyst Characterization

We characterized the natural zeolite and K/NZ catalyst porosity by using nitrogen adsorption-desorption isotherm at 77.35 K in order to determine the BET surface area, total pore volume and average pore diameter. We determined the content of the potassium metal on the K/NZ catalysts by using Atomic Absorption Spectroscopy (AAS). We analyzed the functional groups on the surface of the materials by using the Fourier-transform infrared spectroscopy (FT-IR). X-Ray Diffraction (XRD) technique. This was carried out to confirm the crystalline structure.

### 2.3. Activity Test

As shown in Figure 1, the K/NZ catalyst was tested for the transesterification reaction of the RBO by using a 500 mL three-necked round bottom flask as a batch reactor. Initially, we poured the methanol into the reactor and mixed it with the K/NZ catalyst. The reactor was placed in a water bath on a hot plate magnetic stirrer equipped with a reflux condenser. We used a thermometer to measure the temperature. Then, the mixture was heated up to  $60^\circ\text{C}$ . When the mixture reached this temperature, the RBO was introduced into the reactor which was stirred vigorously to ensure that the mixture was uniform. The reaction temperature was maintained  $60^\circ\text{C}$  during reaction. After a certain time, the reaction was stopped and the K/NZ catalyst was separated from the reaction liquid product by filtering. The liquid product was placed into a funnel in order to separate the methyl ester and glycerol. Under atmospheric temperature, both two phases appeared after 12 hours of separation. The methyl ester was in the upper layer and the glycerol was in the lower layer. Subsequently the distilled water was used to wash the methyl ester and to remove the remaining methanol and glycerol. Finally, any traces of water in the product were removed by heating in the oven for 8 hours at  $110^\circ\text{C}$ . In this study, we investigated the effects of RBO to methanol mole ratio, temperature, and catalyst amount were investigated. We used the following equation to determine the yield of biodiesel by:

$$\text{yield}(\%) = \frac{\text{weight of biodiesel} \times \text{total \% of biodiesel product}}{\text{weight of RBO}} \times 100\% \quad (1)$$

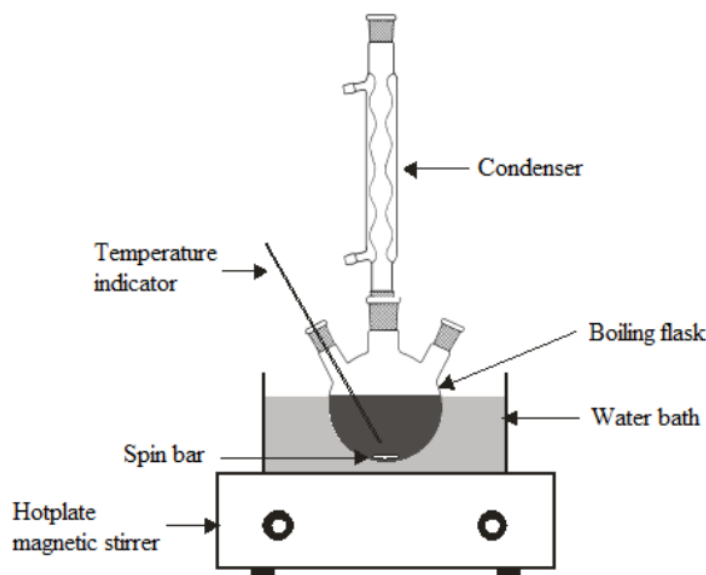


Figure 1 Experiment set-up and apparatus for transesterification reaction of RBO

#### 2.4. Economic Analysis

We conducted an Economic analysis to determine whether or not the project was economically feasible. The Net Present Value (NPV) and Internal Rate of Return (IRR) were evaluated in order to decide the project's feasibility. The calculation of the NPV was based on the difference of present values between the outgoing and incoming cash flows over a certain period of time. Accordingly, the NPV was calculated as follows:

$$NPV = \sum_{i=0}^n \frac{C_i}{(1+r)^i} - C_0 \quad (2)$$

where,  $C_0$  is the capital investment,  $r$  is the Internal Rate of Return (IRR) and  $C_i$  is the cash flow in the  $i$  th year,  $n$  being the lifetime years.

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### 3. RESULTS AND DISCUSSION

#### 3.1. Effect of Inlet Air Temperature

We tested the physico-chemical characteristics of material, including the natural zeolite and K/NZ catalyst by using  $N_2$  adsorption-desorption isotherm, FT-IR spectra and XRD technique. We conducted the  $N_2$  adsorption-desorption isotherm analysis of the raw natural zeolite, activated natural zeolite and K/NZ catalyst in order to determine the BET surface area, total pore volume, and average pore size. Table 1 presents the results. We concluded that the lowest BET surface area was found on the raw natural zeolite ( $34.64 \text{ m}^2 \cdot \text{g}^{-1}$ ). After acid treatment, the BET surface area was increased to  $213.42 \text{ m}^2/\text{g}$  due to the opening of the natural zeolite's internal pores. As well as the BET surface area, after activation from using acid solution, the total pore volume of natural zeolite increased from  $0.1020$  to  $0.1994 \text{ cm}^3 \cdot \text{g}^{-1}$ . On the other hand, the reduction of average pore size diameter occurred from  $11.78$  to  $3.74 \text{ nm}$ . We used the impregnation technique to attach the Potassium metal to the surface of the natural zeolite. The

attachment of Potassium metals to the surface of the catalyst was intended to form an active site which served to accelerate the reaction. After preparing the catalyst by impregnation, the surface area and total pore volume reduced to  $111.56 \text{ m}^2/\text{g}$  and  $0.0789 \text{ cm}^3 \cdot \text{g}^{-1}$  respectively. Meanwhile, the K/NZ catalyst's average pore size diameter increased to  $8.28 \text{ nm}$ . The reactant molecules would have easy access to the internal catalyst when there was, on average, a large sized pore size diameter.

Table 1 Characteristics of raw natural zeolite, activated natural zeolite and K/NZ catalyst

Sampel	BET surface area ( $\text{m}^2 \cdot \text{g}^{-1}$ )	pore size (nm)	total pore volume ( $\text{cm}^3 \cdot \text{g}^{-1}$ )
Raw natural zeolite	34.64	11.78	0.1020
Activated natural zeolite	213.42	3.74	0.1994
K/NZ catalyst	111.56	8.28	0.0789

We used the X-Ray Diffraction (XRD) analysis to evaluate respectively the crystalline structure of activated natural zeolite and K/NZ catalyst. Figures 2a and 2b show the results of the XRD analysis of the activated natural zeolite and the K/NZ catalyst.

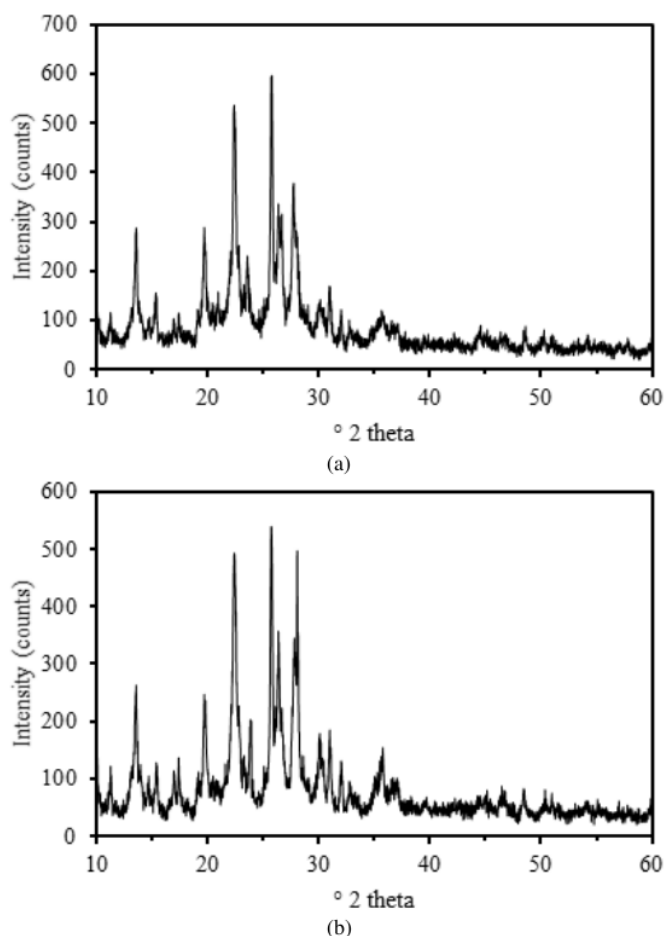


Figure 2 XRD pattern of: (a) activated natural zeolite; and (b) K/NZ catalyst

The XRD pattern of activated natural zeolite exhibits the typical diffraction peaks of zeolite at Bragg angle ( $2\theta$ ) = 12.4°; 19.4°; 29.9°; 37.1°; 45°; 56°; and 60.6°. The pattern indicates, also, that the natural zeolite, used in this study, was grouped into a mordenite type. The K/NZ catalyst displayed a new phase of Potassium oxide ( $K_2O$ ) species in  $2\theta = 31^\circ$ ; 39°; 51° and 55° which corresponded to (1 1 7), (2 2 0), (6 3 1), and (7 2 0) planes. The  $K_2O$  species was formed during the calcination process. Kusuma et al. (2013) indicated that the  $K_2O$ 's contribution was to increase catalytic activity during the transesterification reaction due to it providing the basicity of a solid surface.

We determined the Potassium content in the activated natural zeolite and the K/NZ catalyst by using Atomic Absorption Spectroscopy (AAS) and the results for the modified zeolite and the K/NZ catalyst were 0.34% (weight) and 4.76%, respectively. The result showed that the Potassium content on the modified zeolite increased after its impregnation with  $KNO_3$ . This indicated that, during the impregnation process, the Potassium molecules were attached or incorporated into zeolite structure or matrix.

Figure 3 compares the FT-IR spectra of the activated natural zeolite and the K/NZ catalyst. The FT-IR spectra showed a band at 1640  $cm^{-1}$  which were attributed to the scissor vibrations in water molecule as shown in Figure 3. The asymmetric and symmetric stretching vibrations on wavelength of 706 and 1050  $cm^{-1}$  corresponded to  $SiO_4$  and AlO structures respectively. The aim of the activation of the raw natural zeolite was to eliminate the mineral impurities on the internal pores of materials and to reduce the content of aluminum (Al) in the framework (dealumination). The dealumination could result in the active sites that had high acid strength. The wavenumber on 1041 to 1080  $cm^{-1}$  indicated the shifted asymmetric stretching vibration of Si-O-Al. Due to the Al framework being reduced to become the Al non framework (dealumination), the wavenumber shifted to a larger band caused, also, the zeolite's internal pore to be more open and clean from impurities. The band at 550  $cm^{-1}$  was associated to the deformation vibration of Al-O-Si group. The stretching of the zeolitic structure's hydroxyl groups was shown at the broad peak on 3400–3700  $cm^{-1}$ . Meanwhile, the intensity of the O-H stretching vibration (3464  $cm^{-1}$ ) and O-H bending vibration (1635  $cm^{-1}$ ) declined after the activation.

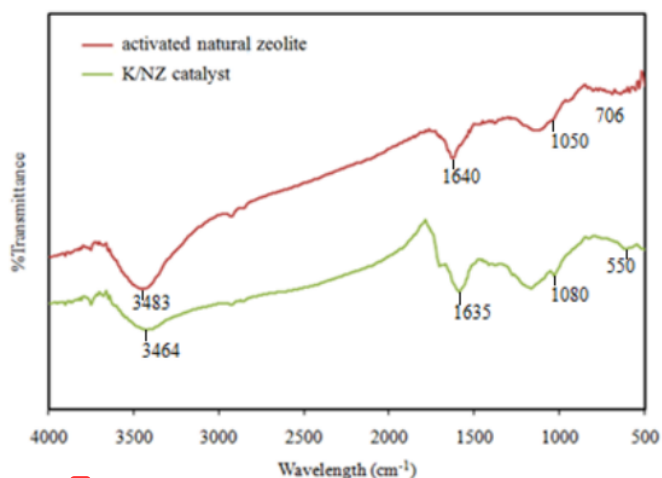
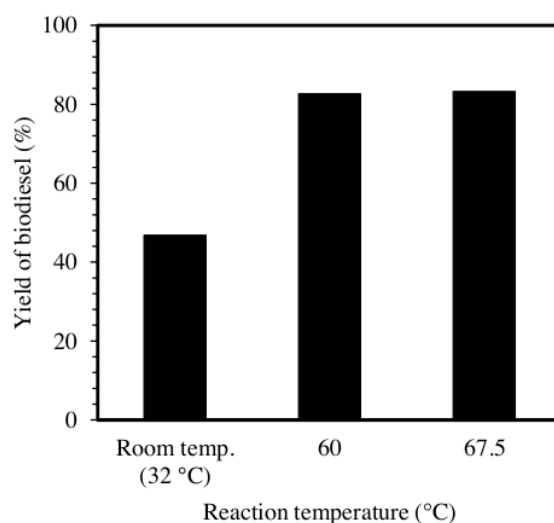


Figure 3 The FT-IR spectra of activated natural zeolite and K/NZ catalyst

## 3.2. Transesterification Reaction

### 3.2.1. Effect of reaction temperature

We tested the K/NZ catalyst for transesterification reaction by using methanol and RBO as feedstock. We conducted the transesterification reaction by using three different reaction temperatures to study the effect of reaction temperatures on biodiesel yield. Figure 4 presents the results. As can be seen in Figure 4, the reaction temperatures affected the biodiesel yield. When the reaction temperature was elevated from room temperature (32°C) to 60°C, the biodiesel yield increased from 46.8% to 82.6%. It can be explained that the increased reaction temperature accelerated the rate of reaction and increased the biodiesel yield. There was, also, a further increase in the reaction temperature to methanol reflux temperature (67.5°C) whereby the biodiesel yield increased slightly to 83.2%. A slight increase in biodiesel yield was due to the reflux conditions which formed the vapor phase. This caused the rate of reaction rate to be constant due to the effect of mass transfer. The increasing of the reaction temperature reduced the oil's viscosity and resulted in better mixing of oil with methanol and the separation of glycerol from biodiesel occurred faster.



4  
Figure 4 The effect of reaction temperature on the biodiesel yield (reaction time between 4 h, amount of catalyst used was 5 wt.% of RBO, and RBO to ratio methanol 1:12)

### 3.2.2. Effect of RBO to methanol mole ratio

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The transesterification is a reversible reaction. Moreover, it consists of three consecutive reversible reactions. As per Le Chatelier's principle, biodiesel yield can be enhanced by increasing the reactant concentration so that the reaction equilibrium shifts to the right side as the product forms. Methanol is widely used because its reaction with triglycerides runs faster and provides a higher conversion in a shorter time when compared to other alcohols. Furthermore, the long-chain alcohols are easily contaminated by water. The oil to methanol stoichiometric mole ratio was 1:3. Thus, in order to shift the reaction equilibrium to the right side the methanol to oil stoichiometric mole ratio ought to be larger than that of stoichiometric mole ratio. We applied the high methanol to oil mole ratio in order to increase the miscibility and to reduce the mass transfer limitation in the alcohol and oil phase. In this study, the RBO to methanol mole ratio was varied to 1:6, 1:8, 1:10 and 1:12, respectively. Figure 5 describes the effect of RBO to methanol mole ratio on the biodiesel yield. As shown in Figure 5, by using mole ratios of 1:6 and



1:8, biodiesel yields were 62.4% and 70.8% respectively. Then, by using the mole ratios of 1:8 and 1:10, the biodiesel yield was increased to 74.1% and 81.9% respectively at. The highest biodiesel yield was obtained at RBO to methanol by using a mole ratio of 1:12.

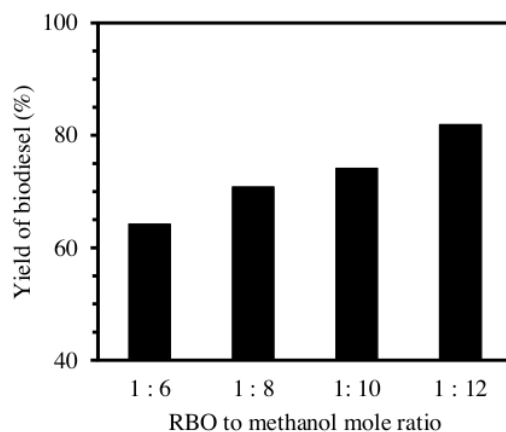


Figure 5 The effect of RBO to methanol mole ratio on the yield of biodiesel (reaction time between 4 h, amount of catalyst used was 55 wt.% of RBO, and reaction temperature was on 60°C)

### 3.2.3. Effect of the amount of catalyst

The amount of catalyst, required for biodiesel production, has a significant impact on the cost of production and the environment. The use of large amounts of catalysts in transesterification reaction increases the rate of reaction to achieve higher biodiesel yields. However, in order to reduce the cost of production, it is preferable to apply the minimum amount of catalyst and the minimum amount of chemicals. It is observed from Figure 6 that, when the amount of the catalyst increases from 0.5 to 5 wt.% of RBO increased the biodiesel yield. The highest biodiesel yield was 81.9% which was obtained when the catalyst amount was 5 wt.% of RBO. The increases to the amounts of the catalysts enhances the availability and number of catalytically active sites and, in turn, increases the biodiesel yield.

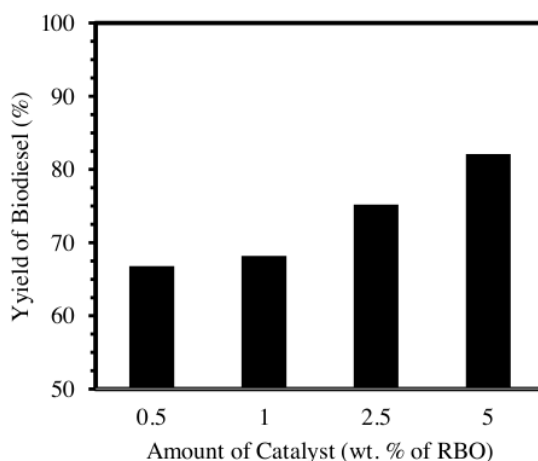


Figure 6 The effect of amount of catalyst on the yield of biodiesel (reaction time 4 h, RBO to methanol ratio 1:12, and reaction temperature was on 60°C)

### 3.2.4. Catalyst reusability

The reusability of catalyst is an important factor in the sustainability of using heterogeneous catalysts for biodiesel production. Prior to reuse, the K/NZ catalysts were regenerated by washing them in n hexane to remove the remaining impurities on the catalyst's surface and internal pore. The transesterification reaction was carried out under constant operating conditions (reaction time 4 hours, RBO to methanol ratio 1:12, and reaction temperature was on 60°C). As shown in Figure 7, the biodiesel yield was found to be 81.9% (first use), 62.8% (second use) and 52.3% (third use). The reduction of biodiesel yield could be because of the leaching of active sites on the catalysts' surfaces. Leaching of the active phase to the alcoholic phase can be attributed to the bond breaking and formation of  $K^+$  and  $CHO^-$  (Baroutian et al., 2011).

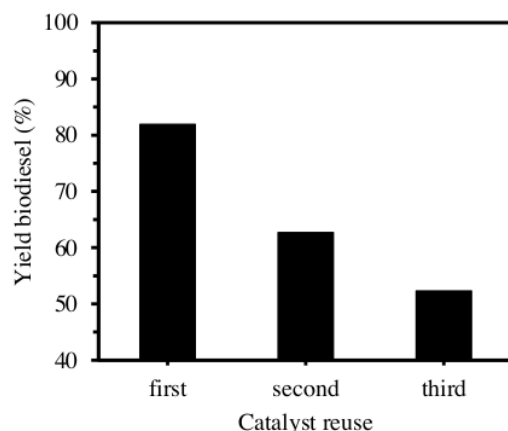


Figure 7 The reusability of the K/NZ catalyst (reaction time 4 h, RBO to methanol mole ratio 1:12, the amount of catalyst of 5 wt.% RBO, and reaction temperature was on 60°C)

### 3.3. Economic Analysis

We performed an economic analysis by using the NPV method for the biodiesel production project. The basis of the project's capital investment is determined on the manufacturing cost and the working capital. The manufacturing cost comes mainly from the cost of raw materials (RBO, methanol, catalyst, chemicals, etc.), labor and utilities (steam, water, electricity). As by-product, Glycerol has great value in some industries and, thus, it was considered that there was revenue to be obtained from the glycerol generated in the project. The length of the project is 10 years and the annual bank interest rate is 12.5% per year. Table 2 presents the results of the economic analysis.

Table 2 Economic analysis

Parameters	Value
Total biodiesel production (tons/year)	80,400
Lifetime of project (year)	10
Net Present Value (IDR)	372,326,000,000
Internal Rate of Return	16.66%
Break Even Point (BEP)	57.64%
Biodiesel cost (IDR/liter)	10,300

As shown in Table 2, the NPV and the IRR resulted in a profitable investment due to the project's NPV being greater than its capital cost and the IRR was 1.5 times higher than the bank interest

rate (6.5%). A project with a higher NPV is considered to be more interesting because it indicates that the project's projected generated earnings generated exceed the predicted costs. The NPV assists, also, in evaluating a project realistically. The greater the IRR, the greater the project is assessed to be potentially economic since the IRR refers to the return which can be earned on the capital invested in the project. The project's Break-Even Point (BEP) value was achieved at 57.64% with a capacity of 80,400 tons/year. The BEP is the point at which the product stops costing money to produce and sell and starts to generate a profit for the company. At the BEP, the production costs equal income from sales.

The cost of biodiesel is calculated by dividing total operating costs with the total cost of soybean oil productivity. The cost of biodiesel, produced from the RBO, was higher than that from petroleum diesel. The Indonesian Government's policies can influence greatly the competitiveness of biodiesel fuel relative to petroleum diesel strongly. In order to commercialize biodiesel, there is a need to pay subsidies since the biodiesel prices are comparatively higher than those of petroleum fuel. Furthermore, the Indonesian Government has to interfere in to the market through regulating and supporting the private sector companies in the form of infrastructure, tax and reduction of commodity prices. The farmer support programs were intensified, also, to promote the growth of biodiesel in the domestic market. The use of biodiesel was driven by increasing the annual road tax which drivers had to pay when using petroleum diesel due to the negative impact of diesel engines' emissions on the environment.

#### 4. CONCLUSION

In order to study and optimize the reaction conditions, the transesterification reaction of RBO using K/NZ catalysts were conducted by varying many parameters such as reaction temperature, RBO to methanol mole ratio, and catalyst amount. The optimal conditions were reaction temperature of 67.5°C, RBO to methanol mole ratio of 1:12, and catalyst amount of wt.5%. RBO. Under the obtained optimum conditions, the biodiesel yield was 83.2%. This indicated that potassium supported on natural zeolite (the K/NZ catalyst) could be used as a catalyst for the transesterification of RBO. The K/NZ catalyst could be reused up to 3 times for esterification reactions; however, this reduced the biodiesel yield to 52.3%.

#### 5. ACKNOWLEDGEMENT

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